

# Rigid Body dynamics

(1)

Size and shape don't change.

$$\vec{P} = \sum m_i \vec{\dot{r}}_i \quad \text{position of COM} \quad \vec{J} = \sum m_i \vec{r}_i \wedge \vec{\dot{r}}_i \quad \text{omit indices}$$

Motion of COM:  $\vec{P} = M\vec{R} = \sum \vec{F}_i$  ← external forces

Rotational Motion:  $\vec{J} = \sum \vec{r}_i \wedge \vec{F}_i$  ← External forces  
Assume internal forces are central.

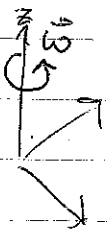
ie.  $\vec{J} = \sum_i m_i \vec{r}_i \wedge \vec{\dot{r}}_i = \sum_i \sum_j \vec{r}_i \wedge \vec{F}_{ij} + \sum_i \vec{r}_i \wedge \vec{F}_i$

NB.  $\vec{r}_i \wedge \vec{r}_i = 0$   
so only  $\vec{r}_i \wedge \vec{\dot{r}}_i$  remains

$= 0$   
if forces are central

ie.  $\vec{r}_1 \wedge \vec{F}_{12} + \vec{r}_2 \wedge \vec{F}_{21} = \vec{r}_1 \wedge \vec{F} - \vec{r}_2 \wedge \vec{F} = \vec{r} \wedge \vec{F} = 0$   
if central  
↑  $F_{21} = -F_{12}$

## Rotation about an axis



cylindrical polars  $(\rho, \phi, z)$   $\omega = \dot{\phi}$

$$J_z = \sum m \rho v_\phi = \sum m \rho^2 \omega = I \omega$$

↓  $v = r\omega$

$I = \sum m \rho^2$  moment of inertia

$\vec{J}_z = I \dot{\omega} = \sum \rho F_\phi$  ← constant  
equ of motion of rotating body

$T = \sum \frac{1}{2} m (\rho \dot{\phi})^2 = \frac{1}{2} I \omega^2$

# Reaction at the axis [Not covered in class]

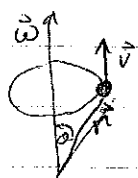
(2)

$\dot{J}_z = I \dot{\omega} = \sum r F_\phi$  does not include reaction of axis because the axis is at  $\rho = 0$  and cannot exert a torque.

Go back to  $\sum \vec{P} = M \vec{R} = \vec{Q} + \sum \vec{F}$

$\underbrace{\vec{Q}}_{\text{force on body at axis}} + \underbrace{\sum \vec{F}}_{\text{all other forces}}$

Now,  $\vec{v} = \vec{\omega} \wedge \vec{r} \Rightarrow \dot{\vec{r}} = \vec{\omega} \wedge \vec{r}$

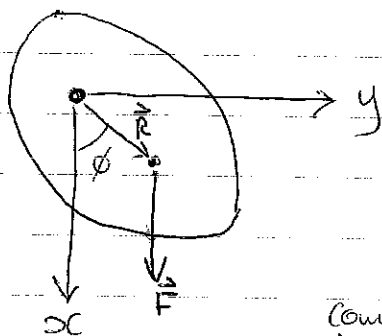


$\Rightarrow \dot{\vec{r}} = \vec{\omega} \wedge \vec{r} + \vec{\omega} \wedge (\vec{\omega} \wedge \vec{r}) = \underbrace{\vec{\omega} \wedge \vec{r}}_{\text{tangential acceleration in } \phi \text{ direction}} + \underbrace{\vec{\omega} \wedge (\vec{\omega} \wedge \vec{r})}_{\text{radial acceleration}}$

Combine above eqns to find  $\vec{Q}$

## Example Solid body pendulum

Take z-axis as axis of rotation



$\vec{F} = (Mg, 0, 0)$  acts at COM

$I \ddot{\phi} = -MgR \sin \phi$  (from  $\dot{J}_z = I \dot{\omega} = \sum r F_\phi$ )

Compare simple pendulum

$\ddot{\phi} = -\frac{g}{l} \sin \phi$

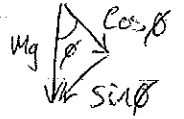
$\Rightarrow$  "l" =  $\frac{I}{MR}$   
length of equivalent simple pendulum

frequency:  $\omega = \sqrt{\frac{g}{l}} = \sqrt{\frac{gMR}{I}}$

Reaction  $\vec{Q}$ :  $\vec{P} = M\vec{R}' = \vec{Q} + \sum \vec{F}_0$  (3)

$$\Rightarrow \vec{Q} = M\vec{R}' - \sum \vec{F}_0$$

$$= M(\dot{\omega} R \vec{R} + \dot{\omega} R (\dot{\omega} R \vec{R})) - Mg \vec{z}$$



$Q_z = 0$  centripetal force provided by pivot

$Q_r = -MR\dot{\phi}^2 - Mg \cos \phi$

$Q_\phi = MR\ddot{\phi} + Mg \sin \phi$

Re-write using  $I\ddot{\phi} = -MgR \sin \phi$  and  $E = \frac{1}{2}I\dot{\phi}^2 - MgR \cos \phi$

$Q_z = 0$

$Q_r = -Mg(1 + R/l)\cos \phi - 2E/l$

$Q_\phi = Mg(1 - R/l)\sin \phi$



purely a function of coords, not velocities and acceleration.  $l = \frac{I}{MR}$   
N.B.  $l > R$

N.B. simple pendulum:  $Q_z = 0$

$Q_r = -ml\dot{\phi}^2 - mg \cos \phi$

$Q_\phi = ml\ddot{\phi} + mg \sin \phi$

but  $\ddot{\phi} = -\frac{g}{l} \sin \phi$

and  $E = \frac{1}{2}ml\dot{\phi}^2 - mgl \cos \phi$

$\Rightarrow ml\dot{\phi}^2 = \frac{2}{l}(E + mgl \cos \phi)$

so  $Q_z = 0$

$Q_r = -3mg \cos \phi - 2E/l$

$Q_\phi = -mg \sin \phi + mg \sin \phi = 0$

(simple pendulum point mass has no extension and so can't spin)

[end of "not covered in class"]

# Perpendicular components of Ang. Mom.

(4)

So far we <sup>only</sup> considered  $J_z$

Cartesian coords:  $\dot{x} = -\omega y$ ,  $\dot{y} = \omega x$ ,  $\dot{z} = 0$

$$J_x = \sum m (-z \dot{y}) = -\sum m x z \omega$$

$$J_y = \sum m (z \dot{x}) = -\sum m y z \omega$$

$$\vec{J} = \vec{r} \wedge \vec{p}$$

$$\begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ x & y & z \\ m\dot{x} & m\dot{y} & m\dot{z} \end{vmatrix} = 0$$

$$= \hat{i} (0 - z m \dot{y}) - \hat{j} (0 - m \dot{x} z) + \hat{k} (x m \dot{y} - y m \dot{x})$$

$$\vec{r} = \vec{\omega} \wedge \vec{r}$$

$$\dot{x} = (\vec{\omega} \wedge \vec{r})_x$$

$$\begin{vmatrix} i & j & k \\ 0 & 0 & \omega \\ \dot{x} & \dot{y} & \dot{z} \end{vmatrix}$$

$$\begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & \omega \\ \dot{x} & \dot{y} & \dot{z} \end{vmatrix} = \hat{i} (-\omega y) - \hat{j} (-\omega x) + \hat{k} 0$$

$$= -\hat{i} \omega y + \hat{j} \omega x$$

So

$$J_x = I_{xz} \omega$$

$$J_y = I_{yz} \omega$$

$$J_z = I_{zz} \omega$$

$$I_{xz} = -\sum m x z$$

$$I_{yz} = -\sum m y z$$

$$I_{zz} = \sum m (x^2 + y^2)$$

previously denoted  $I$ .

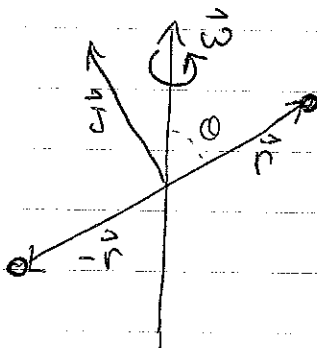
products of inertia

Moment of inertia about z-axis

Note: not constants!  $\dot{I}_{xz} = -\omega I_{yz}$ ,  $\dot{I}_{yz} = \omega I_{xz}$ ,  $\dot{I}_{zz} = 0$

i.e.  $\dot{I}_{xz} = -\sum m \dot{x} z$   
but  $\dot{x} = -\omega y$

Example



2 masses connected by light rod, rigidly fixed at angle  $\theta$

$$\vec{J} = m \vec{r} \wedge \dot{\vec{r}} + m (-\vec{r}) \wedge (-\dot{\vec{r}}) = 2m \vec{r} \wedge (\vec{\omega} \wedge \vec{r})$$

$\vec{J}$  is I to  $\vec{r}$

When rod is in  $xz$ -plane, masses move in  $\pm y$  direction  
 $\Rightarrow$  component of A.M. about  $x$ -axis and  $z$ -axis.

~~Note that  $I_{xz}$~~  So  $\vec{J}$  and  $\vec{\omega}$  in general point in different directions!

Special case: products of inertia vanish,  $\Rightarrow \vec{J}$  is in  $z$ -direction  
 $\Rightarrow z$ -axis is called "principal axis of inertia".

e.g.  $z$ -axis is a principal axis when

•  $xy$  plane is a plane of reflection symmetry (contribution to  $I_{xz}$  and  $I_{yz}$  from any part  $(x, y, z)$  cancel with those from  $(x, y, -z)$ )

• if  $z$ -axis is an axis of rotational symmetry  
 $[(x, y, z)$  contribution cancelled by  $(-x, -y, z)]$

For bodies with 3 symmetry axes (e.g. rectangular parallelepiped, ellipsoid) there are 3 ~~principle~~ perpendicular principal axes <sup>[in fact this is always true]</sup>  $\Rightarrow$  <sup>more advantageous to</sup> choose these ~~as~~ coord. axes

We shall ~~no~~ no longer assume  $z$ -axis as axis of rotation.

$$\vec{\omega} = (\omega_x, \omega_y, \omega_z)$$

$$\vec{J} = \sum m \vec{r} \wedge (\vec{\omega} \wedge \vec{r}) = \sum m [r^2 \vec{\omega} - (\vec{r} \cdot \vec{\omega}) \vec{r}]$$

e.g.  $J_x = \sum m [(y^2 + z^2) \omega_x - (xy \omega_y + xz \omega_z)] z$  linear combinations of components of  $\vec{\omega}$

$J_x$	$J_y$	$J_z$	$=$	$I_{xx}$	$I_{xy}$	$I_{xz}$	$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$
$J_y$	$J_x$	$J_z$	$=$	$I_{yx}$	$I_{yy}$	$I_{yz}$	$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$
$J_z$	$J_y$	$J_x$	$=$	$I_{zx}$	$I_{zy}$	$I_{zz}$	$\begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$

inertia tensor  $\underline{I}$

So, e.g.  $\vec{J}_C = I_{Cxx} \omega_x + I_{Cyy} \omega_y + I_{Czz} \omega_z$  etc. (rotor) (6)  
 $\vec{I}$  is symmetric, e.g.  $I_{xy} = I_{yx}$

If coordinate axes are all axes of symmetry

$$\vec{I} = \begin{bmatrix} I_{Cxx} & 0 & 0 \\ 0 & I_{Cyy} & 0 \\ 0 & 0 & I_{Czz} \end{bmatrix} \quad \text{diagonal}$$

then:  $\vec{J}_C = I_{Cxx} \omega_x$ ,  $\vec{J}_y = I_{Cyy} \omega_y$ ,  $\vec{J}_z = I_{Czz} \omega_z$

$\Rightarrow \vec{J}$  is parallel to  $\vec{\omega}$  if  $\vec{\omega}$  is along any <sup>one</sup> of the symmetry axes.

In fact, ~~for~~ any symmetric tensor can be diagonalised  
 $\Rightarrow$  any rigid body has three perpendicular axes through any given point which are principal axes of inertia.

then  $\vec{\omega} = \omega_1 \hat{e}_1 + \omega_2 \hat{e}_2 + \omega_3 \hat{e}_3$  {  $\hat{e}_1, \hat{e}_2, \hat{e}_3$  }

unit vectors along principle axes

$$\Rightarrow \vec{J} = I_1 \omega_1 \hat{e}_1 + I_2 \omega_2 \hat{e}_2 + I_3 \omega_3 \hat{e}_3$$

$I_1, I_2, I_3$  = principal moments of inertia (3 diagonal elements of  $\vec{I}$ )  
 $\uparrow$  single subscript distinguishes them from moments of inertia about arbitrary axes.

Note: Principal axes are fixed in body and define a rotating frame.  
 Principal moments  $I_1, I_2, I_3$  are <sup>then</sup> constants.

$$T = \sum \frac{1}{2} m \dot{r}^2 = \sum \frac{1}{2} m (\vec{\omega} \wedge \vec{r})^2 = \sum \frac{1}{2} m [\omega^2 r^2 - (\vec{\omega} \cdot \vec{r})^2] \quad (8)$$

(by vector algebra)

$$\Rightarrow T = \frac{1}{2} \vec{\omega} \cdot \vec{J}$$

$$\Rightarrow T = \frac{1}{2} I_1 \omega_1^2 + \frac{1}{2} I_2 \omega_2^2 + \frac{1}{2} I_3 \omega_3^2$$

cf  $T = \frac{1}{2} M v^2 = \frac{1}{2} \vec{v} \cdot \vec{p}$

different "masses" in different directions.

### Symmetric bodies

2 principal moments of inertia coincide, e.g.  $I_1 = I_2$

e.g. if  $\hat{e}_3$  is a symmetry axis. (cylindrical symmetry or axis of more than 2-fold rotational symmetry, e.g. equilateral triangular prism, or square pyramid. - see back p 87)

then  $\vec{J} = I_1 (\omega_1 \hat{e}_1 + \omega_2 \hat{e}_2) + I_3 \omega_3 \hat{e}_3$

If  $\omega_3 = 0$ ,  $\vec{J} = I_1 \vec{\omega}$ , so  $\vec{J}$  is parallel to  $\vec{\omega}$ .

Any axis in plane of  $\hat{e}_1$  and  $\hat{e}_2$  is a principal axis.

$\Rightarrow$  choose any pair of orthogonal axes in plane normal to  $\hat{e}_3$ .

$\Rightarrow$  they need not even be fixed in body provided they remain orthogonal to themselves and  $\hat{e}_3$ .

Totally symmetric:  $I_1 = I_2 = I_3$  sphere, cube, ~~the~~ regular tetrahedron

$\vec{J} = I \vec{\omega}$  whatever direction  $\vec{\omega}$  takes, so every axis is a principal axis.

N.B. see sec 9.5 for calculation of Moments of inertia

## Effect of a small force on axis

(8)

- Assume rigid body can rotate about a fixed pivot, i.e. only one pt on axis is fixed

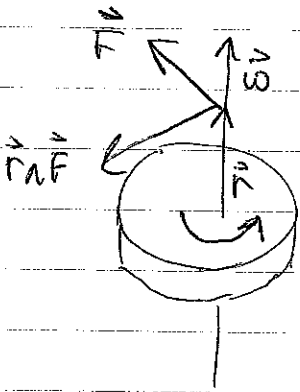
- Assume initially body is freely rotating about a principal axis,  $\hat{e}_3$ .

$$\Rightarrow \vec{\omega} = \omega \hat{e}_3$$

$$\vec{J} = I_3 \omega \hat{e}_3$$

No external force:  $\dot{\vec{J}} = I_3 \dot{\vec{\omega}} = 0$  [from  $\vec{J} = I_1 \omega_1 \hat{e}_1 + I_2 \omega_2 \hat{e}_2 + I_3 \omega_3 \hat{e}_3$ ]  
 $\Rightarrow$  axis fixed in space and  $\vec{J}$  and  $\vec{\omega}$  are constant (not true if axis of rotation was not a principal axis)

Apply <sup>small</sup> force  $\vec{F}$  to axis at pt  $\vec{r}$



Eqn of motion  $\dot{\vec{J}} = \vec{r} \wedge \vec{F}$

$\Rightarrow$  Axis changes direction

$\Rightarrow$  Small component of  $\vec{\omega}$  perpendicular to  $\hat{e}_3$

small  $F \Rightarrow |\delta \vec{\omega}|$  small in comparison to  $|\vec{\omega}|$   
 i.e. angular velocity with which axis moves is small in comparison to angular velocity about axis  
 $\Rightarrow$  ignore components of  $\vec{J}$  normal to axis of rotation.

$$\Rightarrow \vec{J} = I_3 \dot{\vec{\omega}} = \underbrace{\vec{r} \wedge \vec{F}}_{\text{torque}}$$

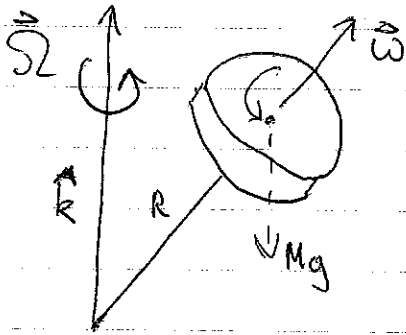
$\vec{r} \wedge \vec{F}$  is  $\perp$  to  $\vec{\omega}$ , so  $|\vec{\omega}|$  does not change ( $\frac{d|\vec{\omega}|}{dt} = 2\vec{\omega} \cdot \dot{\vec{\omega}}$ )

but direction of  $\vec{\omega}$  does change. Axis will move in direction  $\vec{r} \wedge \vec{F}$  which is  $\perp$  to  $\vec{F}$ .



Example Precession of spinning top / gyroscope.

(9)



$$\vec{F} = -Mg \hat{k} \quad \text{acts on COM}$$
$$\text{at } \vec{R} = R \hat{e}_3$$

$$\Rightarrow I_3 \dot{\omega} \hat{e}_3 = -MgR \hat{e}_3 \wedge \hat{k} \quad (I_3 \dot{\omega} = r \wedge F)$$

$$\text{cf. } \dot{\hat{e}}_3 = \vec{\Omega} \wedge \hat{e}_3$$

$$\Rightarrow \vec{\Omega} = \frac{MgR}{I_3 \omega} \hat{k} \quad \text{Angular velocity of precession.}$$

Note  $\Omega$  is independent of angle of inclination

Treatment valid if  $\Omega \ll \omega$

$$\text{i.e. } MgR \ll I_3 \omega^2$$

i.e. rotational KE  $\gg$  change in gravitational potential

$$T = \frac{1}{2} I_3 \omega^2 \gg MgR$$

$\Omega$  is small if  $I_3$  and  $\omega$  are big

# Instantaneous Angular Velocity

(10)

For a body that is not rotating about a principal axis small forces not subjected to when rotating about principal axes one can still define an <sup>instantaneous</sup> angular velocity but ~~but~~ in general both its magnitude and direction change in time.

First consider a body rotating freely about a <sup>fixed</sup> pivot.  
 $\Rightarrow$  position of every point of body is <sup>fixed</sup> if we specify it using the three principal axes <sup>relative to</sup> (actually true for any three axes fixed in body - but convenient choice is principal axes)  $\vec{r} = r_1 \vec{e}_1 + r_2 \vec{e}_2 + r_3 \vec{e}_3$

Velocity of pt is determined by  $\dot{\vec{e}}_1, \dot{\vec{e}}_2, \dot{\vec{e}}_3$   
 $\dot{\vec{r}} = r_1 \dot{\vec{e}}_1 + r_2 \dot{\vec{e}}_2 + r_3 \dot{\vec{e}}_3$

Can show that we can always define an instantaneous  $\vec{\omega}$  no matter how body is moving:

Define  $a_{ij} = \vec{e}_i \cdot \dot{\vec{e}}_j$   
 $\vec{e}_i \cdot \vec{e}_i = 1$  etc

so  $0 = \frac{d}{dt} (\vec{e}_1 \cdot \vec{e}_1) = 2 \vec{e}_1 \cdot \dot{\vec{e}}_1 = 2a_{11}$

so  $\dot{\vec{e}}_1$  must have form

$$\dot{\vec{e}}_1 = a_{21} \vec{e}_2 + a_{31} \vec{e}_3$$

[check  $\vec{e}_2 \cdot \dot{\vec{e}}_1 = a_{21}$  and  $\vec{e}_3 \cdot \dot{\vec{e}}_1 = a_{31}$ ]

Also  $0 = \frac{d}{dt} (\vec{e}_1 \cdot \vec{e}_2) = \dot{\vec{e}}_1 \cdot \vec{e}_2 + \vec{e}_1 \cdot \dot{\vec{e}}_2 = a_{21} + a_{12}$

So can define a vector  $\vec{\omega} = \omega_1 \hat{e}_1 + \omega_2 \hat{e}_2 + \omega_3 \hat{e}_3$  (11)

where

$$\omega_1 = -a_{23} = a_{32}$$

$$\omega_2 = -a_{31} = a_{13}$$

$$\omega_3 = -a_{12} = a_{21}$$

for then

$$\begin{aligned} \dot{\hat{e}}_1 &= \omega_3 \hat{e}_2 - \omega_2 \hat{e}_3 = a_{21} \hat{e}_2 + a_{31} \hat{e}_3 \\ &= \omega_3 \hat{e}_2 - \omega_2 \hat{e}_3 \\ &= \vec{\omega} \wedge \hat{e}_1 \end{aligned}$$

$$\begin{vmatrix} \hat{e}_1 & \hat{e}_2 & \hat{e}_3 \\ \omega_1 & \omega_2 & \omega_3 \\ 0 & 0 & 0 \end{vmatrix} = \hat{e}_1(0) - \hat{e}_2(-\omega_3) + \hat{e}_3(-\omega_2) \quad \text{as req'd}$$

Combining with

$$\begin{aligned} \dot{\hat{e}}_2 &= \vec{\omega} \wedge \hat{e}_2 \\ \dot{\hat{e}}_3 &= \vec{\omega} \wedge \hat{e}_3 \end{aligned}$$

gives

$$\boxed{\dot{\vec{r}} = \vec{\omega} \wedge \vec{r}} \quad \left[ \vec{r} = r_1 \hat{e}_1 + r_2 \hat{e}_2 + r_3 \hat{e}_3 \right]$$

(velocity of any pt in body) ↓ sub in  $\dot{\hat{e}}_i = \vec{\omega} \wedge \hat{e}_i$

$$\begin{aligned} \dot{\vec{r}} &= r_1 \vec{\omega} \wedge \hat{e}_1 + r_2 \vec{\omega} \wedge \hat{e}_2 + r_3 \vec{\omega} \wedge \hat{e}_3 \\ &= \vec{\omega} \wedge (r_1 \hat{e}_1 + r_2 \hat{e}_2 + r_3 \hat{e}_3) \\ &= \vec{\omega} \wedge \vec{r} \end{aligned}$$

So instantaneous angular velocity vector

$\vec{\omega}$  always exists. (instantaneous axis of rotation)

Now consider general case: no pt in body is fixed.

Specify position of body by  $\vec{R}$  (com position) and by orientations of principal axes at  $\vec{R}$ . Then define  $\vec{\omega}$  relative to  $\vec{R}$ .

$\vec{R}$  = velocity of COM

(12)

velocity of pt :  $\vec{v} = \vec{R} + \dot{\vec{r}}^*$   
↑ position relative to COM

But  $\vec{r}^*$  is fixed in body so can same argument as above to define instantaneous angular velocity  $\vec{\omega}$

$\dot{\vec{v}} = \dot{\vec{R}} + \vec{\omega} \wedge \vec{r}^*$   
↑ no star because  $\vec{\omega}$  is independent of origin of coord  
e.g. if body is rotating with  $\vec{\omega}$  about a

fixed pivot :

$$\dot{\vec{v}} = \vec{\omega} \wedge \vec{r} = \vec{\omega} \wedge \vec{R} + \vec{\omega} \wedge \vec{r}^*$$

~~but~~  
but  $\dot{\vec{R}} = \vec{\omega} \wedge \vec{R}$

$$\text{so } \underbrace{\dot{\vec{v}} - \dot{\vec{R}}}_{= \dot{\vec{r}}^*} = \vec{\omega} \wedge \vec{r}^*$$

so  $\vec{\omega}$  is same also relative to COM.

Eqn of motion for rigid body about fixed pivot :

$$\vec{J} = \sum \vec{r} \wedge \vec{F}$$

where  $\vec{J} = I_1 \omega_1 \hat{e}_1 + I_2 \omega_2 \hat{e}_2 + I_3 \omega_3 \hat{e}_3$

In general case we need to know both velocity of COM and  $\vec{\omega}$

Motion of COM

$$\vec{P} = M \vec{R} = \sum \vec{F}$$

Rotational  
motion

$$\vec{J}^* = \sum \vec{r}^* \wedge \vec{F}$$

$\vec{J}^*$  = ang. mom. about COM

$$\vec{J}^* = I_1^* \omega_1 \hat{e}_1^* + I_2^* \omega_2 \hat{e}_2^* + I_3^* \omega_3 \hat{e}_3^*$$

$\hat{e}_1^*, \hat{e}_2^*, \hat{e}_3^*$  = principal axes at centre of mass  
and  $I_1^*, I_2^*, I_3^*$  are corresponding principal moments.

# Rotation about a principal Axis

(14)

Principal axes  $\hat{e}_1, \hat{e}_2, \hat{e}_3$  rotate with body  $\rightarrow$  rotating frame.

$$\frac{d\vec{J}}{dt} = \text{relative absolute}$$

$$\dot{\vec{J}} = \text{relative}$$

Absolute  $\frac{d\vec{J}}{dt} = \sum \vec{r}_i \wedge \vec{F}_i = \vec{\tau}$

(argument below applies equally to body rotating about fixed pivot or COM.)

relative  $\dot{\vec{J}} = I_1 \dot{\omega}_1 \hat{e}_1 + I_2 \dot{\omega}_2 \hat{e}_2 + I_3 \dot{\omega}_3 \hat{e}_3$  ( $I_1, I_2, I_3 = \text{consts}$ )

relation:  $\frac{d\vec{J}}{dt} = \underbrace{\dot{\vec{J}}}_{\text{rate of change in frame}} + \underbrace{\vec{\omega} \wedge \vec{J}}_{\text{rotational change of } \vec{J} \text{ due to rotation of frame}} = \vec{\tau}$

In terms of components:  $I_1 \dot{\omega}_1 + (I_3 - I_2) \omega_2 \omega_3 = \tau_1$

(The Euler equations)

$$I_2 \dot{\omega}_2 + (I_1 - I_3) \omega_3 \omega_1 = \tau_2$$

$$I_3 \dot{\omega}_3 + (I_2 - I_1) \omega_1 \omega_2 = \tau_3$$

Can solve for  $\omega_1(t), \omega_2(t), \omega_3(t)$ .

-but not so useful if external forces are specified in terms of components wrt a fixed set of axes.

(Even if force is const,  $\{F_1, F_2, F_3\}$  depend on ~~vector~~ <sup>time, i.e.</sup> orientation of body) ~~but we can only know by solving~~

... consider free rotation in example below (use Lagrange's eqns for  $\vec{\tau} \neq 0$ .)

# Tennis racket theorem

(15)

Rigid body is rotating freely about principal axis,  $\hat{e}_3$ , say.  
Give small displacement - will  $\vec{\omega}$  remain close to  $\hat{e}_3$ ?

If displacement is small, treat  $\omega_1$  and  $\omega_2$  as small  
and  $\omega_1, \omega_2 \ll \omega_3$ .

then 3rd eqn  $I_3 \dot{\omega}_3 \approx 0$  ( $\tau_3 = 0$ )  
 $\Rightarrow \omega_3 = \text{const.}$

Solve other two eqns by putting  $\omega_1 = a_1 e^{pt}$ ,  $\omega_2 = a_2 e^{pt}$

$$\Rightarrow I_1 p a_1 + (I_3 - I_2) \omega_3 a_2 = 0$$

$$I_2 p a_2 + (I_1 - I_3) \omega_3 a_1 = 0$$

eliminate  $\frac{a_1}{a_2}$

$$\Rightarrow p^2 = \frac{(I_3 - I_2)(I_1 - I_3)}{I_1 I_2} \omega_3^2$$

If  $I_3 > I_1$  and  $I_3 > I_2$

or  $I_3 < I_1$  and  $I_3 < I_2$

}  $p = \text{imaginary} \Rightarrow \text{oscillatory solutions}$

$I_1 > I_3 > I_2$

or  $I_1 < I_3 < I_2$

} real roots

$\Rightarrow \omega_1$  and  $\omega_2$  exponentially increasing.

$\Rightarrow$  motion is stable if  $I_3$  is largest or smallest principal moment.

## Euler's Angles $(\theta, \phi, \psi)$

(16)

$e_1^n, e_2^n, e_3^n$  initially coincide with  $i, j, k$

① Rotate about axis  $k^n$  by angle  $\phi$   
 $\Rightarrow e_1^n, e_2^n, k^n$

② Rotate about the axis  $e_2^{n'}$  by angle  $\theta$   
 $\Rightarrow e_1^{n'}, e_2^{n'}, e_3^n$

③ Rotate about  $e_3^n$  by angle  $\psi$   
 $\Rightarrow e_1^y, e_2^y, e_3^y$

Angular velocity



# Summary

Rotation  
About  
axis

$$\vec{J} = \sum m \vec{r} \wedge (\vec{\omega} \wedge \vec{r}) = \sum m [r^2 \vec{\omega} - (\vec{r} \cdot \vec{\omega}) \vec{r}]$$

linear in  $\vec{\omega}$

Cartesian  
coord

$$\begin{bmatrix} J_x \\ J_y \\ J_z \end{bmatrix} = \underbrace{\begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{bmatrix}}_{\vec{I} \text{ symmetric}} \begin{bmatrix} \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$$

e.g.  $J_x = I_{xx} \omega_x + I_{xy} \omega_y + I_{xz} \omega_z$

If coord axes are axes of symmetry

$$\vec{I} = \begin{bmatrix} I_{xx} & & \\ & I_{yy} & \\ & & I_{zz} \end{bmatrix}$$

$$J_x = I_{xx} \omega_x \quad J_y = I_{yy} \omega_y \quad J_z = I_{zz} \omega_z$$

$\Rightarrow \vec{J}$  parallel to  $\vec{\omega}$  if  $\vec{\omega}$  is along any one symmetry axis

If coord axes are not axes of symmetry: diagonalise  $\Rightarrow \hat{e}_1, \hat{e}_2, \hat{e}_3$

Then can write  $\vec{\omega} = \omega_1 \hat{e}_1 + \omega_2 \hat{e}_2 + \omega_3 \hat{e}_3$  this is basis

$$\text{then } \vec{J} = I_1 \omega_1 \hat{e}_1 + I_2 \omega_2 \hat{e}_2 + I_3 \omega_3 \hat{e}_3$$

$\uparrow \quad \quad \quad \uparrow \quad \quad \quad \uparrow$   
principal moments of inertia